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SIMULATED EARTHQUAKE TESTING OF NATURALLY AGED EXIDE FHC-19 STATION BATTERY CELLS

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A sample of 10-year-old lead-acid storage batteries from the Calvert Cliffs Nuclear Power Station (Baltimore Gas & Electric Company) were tested on a shaker table. Six cells were subjected to simulated earthquakes with a ZPA of approximately 1.5 g. None of the six cells tested showed a significant drop in voltage during the shaker tests. However, only two cells could deliver 80% of their rated capacity following the seismic tests. Two cells were shaken to higher intensities (ZPA approximately equal to 2 g). These cells again provided uninterrupted power during the shaker tests, but had post-seismic capacities that were below the required level for Class 1E battery cells. Four cells were disassembled and examined after the shaker tests. Bus bar material from the positive side of the cells was corroded and brittle (although not cracked) and active material on the positive plates was hard and cracked. Loss of active material from the positive plates is suspected as the main cause of the reduced capacity of the cells.

JC

job	file	date	report no.
740621-108-450	825.92	March 13, 1985	85-51-K

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To Mr. B.A. Oliver
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A sample of 10-year-old lead-acid storage batteries from the Calvert Cliffs Nuclear Power Station (Baltimore Gas & Electric Company) were tested on a shaker table. Six cells were subjected to simulated earthquakes with a ZPA of approximately 1.5 g. None of the six cells tested showed a significant drop in voltage during the shaker tests. However, only two cells could deliver 80% of their rated capacity following the seismic tests. Two cells were shaken to higher intensities (ZPA approximately equal to 2 g). These cells again provided uninterrupted power during the shaker tests, but had post-seismic capacities that were below the required level for Class 1E battery cells. Four cells were disassembled and examined after the shaker tests. Bus bar material from the positive side of the cells was corroded and brittle (although not cracked) and active material on the positive plates was hard and cracked. Loss of active material from the positive plates is suspected as the main cause of the reduced capacity of the cells.

1.0 INTRODUCTION

The large lead-acid storage battery cells that are the subject of this report are used to provide DC power for nuclear power stations under emergency conditions. It is well known that these cells deteriorate with age and it is normal practice to test them at regular intervals to ensure that they are capable

of meeting a specified level of performance. What is not so well understood however, is the effect of age on the mechanical fragility of the cells and whether older cells would be capable of surviving seismic events at the operating basis earthquake (OBE) or safe shutdown earthquake (SSE) levels and to continue to meet the load profile required by the Class 1E system. Because of the importance of storage batteries to the class 1E system, the US Nuclear Regulatory Commission has requested Sandia National Laboratories (SNL) to evaluate the impact of aging and seismic exposure on battery capacity. Ontario Hydro has been sub-contracted to carry out capacity and seismic shaker tests on naturally aged cells supplied by SNL from several US nuclear power stations (SNL Contract 47-4077). The program addresses possible variations between designs produced by different manufacturers.

This report describes the results of a series of experiments carried out at the Ontario Hydro Research Laboratories on a set of ten (10) year old Exide FHC-19 cells from the Calvert Cliffs Nuclear Power Station (Baltimore Gas and Electric Company). The shaker tests were carried out in two stages, with the first stage tests simulating earthquakes with zero-period acceleration levels (ZPA) of about 1.5 g and the second stage tests reaching ZPA levels of about 2g. During the first stage tests, the cells delivered uninterrupted power. However, the discharge tests that followed the shaker tests showed that only two of the six cells could deliver more than 80% of their rated power. During the second stage (high intensity) shaker tests, two cells were tested and both showed a major loss of capacity. To determine the nature of the deterioration of the internal components of the cells, several cells were disassembled for inspection and metallurgical examination. It was found that the active material on the positive plates was hardened and, in many instances, cracked, and that a significant volume of this material had fallen out of the plate grid. Corrosion and brittleness was also noted in the positive bus material.

This report summarizes the tests and results for this batch of cells. A more detailed discussion of the tests and results is contained in references 1, 2 (battery condition and performance), 3 and 4 (seismic test results).

The tests described here were part of a larger program of testing of aged cells. Other cell types tested to date have included Gould FKR (Pickering Nuclear Generating Station)/5,6,7/, Gould NCX2250 (J.A. Fitzpatrick Nuclear Power Station)/8/, Exide EMP-13 (Shippingport Nuclear Power Station/9/ and C&D LCU-13 (North Anna NPS)/10/.

2.0 TEST METHODS AND RESULTS

2.1 Initial Inspection and Conditioning

Ten Exide FHC-19 cells were received from the Calvert Cliffs plant. Except for a small crack on the top plate of one cell, no external damage was found. On the negative plates, regular horizontal and vertical cracks were observed in the sponge lead active material. Small hollow blisters were found near the tops of these plates. The positive plates were bowed (severely in two cells). There was 3 to 5 mm of sediment in the bottoms of the cells, principally lead oxide, but with pockets of lead sulphate. The cells were conditioned (charged and discharged several times to stabilize their condition) and tested for capacity. The electrical state of the cells prior to the seismic tests is summarized in Table 1.

2.2 Seismic Testing - Single Cells

The shaker table and instrumentation used in these experiments is described in Reference 3. The table provides independent motion in three directions. The motion is based on a quasi-random signal, filtered to match the frequency content of a typical earthquake. The duration of each test was 30 seconds. The seismic test method was based on the recommendations of IEEE Std 344-1975 and IEEE Std 501-1978.

For the single cell seismic tests, the cells were mounted individually on the shaker table in a stiff frame, designed to minimize relative motion between the cell jar and the table (see Figure 1). These tests were intended to investigate possible failure modes of internal components. The rig was designed to minimize the danger of jar failure and acid spill. Accelerometers were mounted on the base of the frame and on the top of one of the posts of the cell.

During the seismic tests, the cells were discharged against a resistive load at a 1 h discharge rate. They were considered to have "passed" a seismic test if they remained above 1.75 V during and immediately after the test. The cells were shaken at progressively higher levels up to the machine limit. Each of the four cells that were tested in the single cell frame passed all of the tests. Table 2 provides a log of the test sequence, while Table 3 summarizes the results. There were no sudden drops in cell voltage during any of the shaker tests.

Seismic test results are presented in this report and in References 3 and 4 in terms of acceleration response spectra of the table motion. To provide a convenient means of comparing the acceleration levels encountered during various tests, each test

spectrum is compared to a normalized spectrum defined in IEEE Std 501-1978/11/. The shape of this spectrum is intended to reflect the frequency content of the "typical" seismic environment for electrical equipment. The intensity of the simulated seismic motion is expressed in terms of the ZPA (zero period acceleration) which provides a conservative lower-bound estimate of the peak acceleration of the base.

The single cell tests were conducted in two stages. In the first stage, the shaker table controllers were tuned so that the frequency content of the table motion fitted the standard spectrum shape specified in IEEE Std 501-1978. These tests were carried out in July 1984. Response spectra computed from the base accelerometer outputs are shown in Figures 3 through 14. For the second phase, the controllers were re-adjusted to provide a higher overall level of shaking. These tests took place in December 1984 and involved two cells - #23 which had previously taken part in a rack test, and #51 which had been tested in the single cell frame in July. Spectra from the second phase are shown in Figures 15 through 20.

The higher 'g' levels for the second stage tests were achieved largely by increasing the intensity of mid to high frequency components of the shaker motion (ie. above 5 Hz). The result is a spectrum shape that is rather higher than the standard IEEE 501 shape over the high frequency range. If such a spectrum is compared to the standard shape strictly according to the IEEE 501 methodology, then the ZPA of the fitted spectrum will be a very conservative estimate of the peak accelerations that the cell actually experienced. In this context, it must be recognized that the IEEE Standard is intended to provide a basis for the seismic qualification of a broad range of electrical equipment. The purpose of the experiments described here, however, is not to qualify the cells, but to explore the types of damage that might be inflicted in earthquake motion. Thus, we believe that we are justified in departing from the strict letter of the Standard so that the ZPA values quoted in our results are reasonably close to the peak accelerations encountered during the tests. (See Appendix A for a more complete discussion.) To provide meaningful ZPA data, we have fitted an alternative set of normalized spectra to the experimental data over the 4 Hz to 33 Hz range. These alternative spectra are shown on Figures 15 through 20 as double lines.

2.3 Jar Fragility Test

Earlier testing (Gould NCX2250 cells from J.A. Fitzpatrick Nuclear Power Station/8/) had shown that cracks in the jars would propagate more readily if the cell was mounted loosely in

the test frame. A single test was carried out with an FHC-19 cell loosely mounted in the frame. In this case, the cell jar had no sign of prior cracking and no damage occurred as a result of the test.

2.4 Multi-Cell Rack Test

The single-cell tests were designed to focus on failure modes of internal components. To examine the possible failure modes that would be encountered with normal in-plant mounting arrangements, a shaker test was carried out on a set of three cells mounted on a rack that resembled typical seismically qualified battery racks (see Figure 2). The test log and results are shown on Tables 2 and 3, while test spectra are shown in Figures 21 and 22. No failures occurred during the rack tests.

For practical reasons, the rack that was used for these tests held only three cells. Full scale racks in generating stations are typically much longer. The present tests could be non-conservative, since long strings of cells could, under shaking, impose large impact loads on cells at the end of the string. These tests provide no positive indication that this is a potential source of trouble. Nevertheless, we suggest that in severe seismic environments, it would be beneficial to separate cells into groups of three or so, with rigid partitions on the rack and flexible electrical connections between groups.

2.5 Post-Seismic Capacity Tests and Inspection

Following the shaker table tests the cells were re-tested for electrical capacity. The results of these tests are shown on Table 1. For the first stage tests (ZPA around 1.5 g), there was some loss of discharge capacity for all cells. Only two of the cells had capacities, as measured from the start of the seismic test series, that met the acceptance criterion of more than 80% rated capacity. For the second stage (ZPA around 2 g), the cells both provided uninterrupted power during the seismic tests, but had post-test capacities that were less than 80% of the rated capacity.

For the first stage seismic tests, the capacity tests were done within a few days of the shaker tests. In this case, the test capacity reflected the charge that remained in the cells after the shaking. However, the capacity tests that followed the second stage (higher intensity) seismic tests were delayed for approximately four weeks. Because of our experience with self discharge of aged, seismically damaged cells, we believed that the charge remaining in the cells after this extended wait could be significantly lower than the charge that was available immediately following the shaker test. Accordingly, these two cells were re-charged before the final capacity test. We do not

know at this point how the extra discharge-charge cycle would effect the measured capacity.

Following the seismic tests, four of the cells were disassembled and inspected. Internal components showed various types of age-related damage, including corrosion (bus bars and plates), cracking (positive and negative plates), hardening and loss of active material (positive plates) and gas blistering (negative plates). The degree of damage noted during the post-test inspection correlated with the drop in capacity that occurred because of the simulated seismic shaking.

3.0 CONCLUSIONS

1. The ten year old Exide FHC-19 cells that were the subject of this study showed signs of age related degradation. Some of these signs (plate warping and sedimentation) could be observed from the outside of the cells, while other indications (corrosion damage and brittleness) were discovered when the cells were dissected after the shaker tests.

2. All of the cells that were tested on the shaker table delivered uninterrupted power during repeated strong shaking. There was however significant loss of electrical capacity. Four of the six cells failed to deliver 80% of their rated capacity (the normal acceptance level for emergency power supply batteries) after being shaken to a ZPA level of about 1.5 g. Two cells were shaken to a higher level (ZPA approximately 2 g) and both showed a considerable loss of capacity.

3. Internal components of all of the cells that were disassembled had various types of age related damage, including corrosion, plate swelling, cracking and blistering. The amount of sediment present was uncharacteristically large for lead-calcium alloy cells.

4. There were no signs of damage to the jars during any of the tests. This includes test where a cell was free to move in the test frame (and hence would be subject to impact loads) and tests with multi-cell racks.

4.0 ACKNOWLEDGEMENTS

Test cells and funding for this project were provided by Sandia National Laboratories. This support is gratefully acknowledged. Lloyd Bonzon and Don Hente of SNL are thanked for their large contribution to the project. Within Ontario Hydro, contract coordination was handled by the Electrical Design Department. We are grateful to Colin Royce and Jerry Schendel for their efforts. Much of the testing and analysis was carried out by Brian Aucoin of the Chemical Research Department and Gordon Paulsen of the Mechanical Research Department. Their able work was essential to the successful outcome of the project.

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TABLE 1

CELL CAPACITIES BEFORE AND AFTER SEISMIC TESTING

First Stage Tests - ZPA Approximately 1.5 g

Cell	Time to 1.75 VPC at 3 h Rate Rate (min)			Per Cent of Rated Capacity at 3 h Rate		
	Pre-Seismic	Post-Seismic*	Post-Seismic Plus Seismic**	Pre-Seismic	Post Seismic*	Post-Seismic Plus Seismic**
10	180	104	118	100	58	66
15	155	104	131	86	58	73
23	155	121	135	86	67	75
35	155	121	132	86	67	75
51	170	162	177	94	90	98
57	180	149	164	100	83	91
AVG	166	127	143	92	71	80

Second Stage Tests - ZPA Approximately 2 g

Cell	Time to 1.75 VPC at 3 h Rate Rate (min)		Per Cent of Rated Capacity at 3 h Rate	
	Pre-Seismic	Post-Seismic***	Pre-Seismic	Post Seismic***
23	135	60	75	33
51	176	95	98	53
AVG	155	78	86	43

* Cells not recharged following seismic testing.
** Capacity during seismic test at 1 h rate converted to 3 h capacity and added to post-seismic capacity, as discussed in Reference 1.
***Cells re-charged following second stage seismic tests.

TABLE 2

TEST HISTORY - CALVERT CLIFFS NPP - EXIDE - MODEL FHC-19 CELLS

CELL	DATE	TIME	RUN	XPA X/Y/Z	COMMENTS
Single-Cell Test					
57	July 23/84	2:00	1	0.6/0.5/0.6	No load applied
57	July 23/84	2:02	2	0.6/0.5/0.6	Load on
57	July 23/84	2:03	3	0.8/0.7/0.8	
57	July 23/84	2:05	4	0.9/0.9/1.0	
57	July 23/84	2:07	5	1.1/1.5/1.3	
57	July 23/84	2:10	6	1.3/1.0/1.6	Plotted
15	July 23/84	3:10	1	0.8/0.7/0.8	
15	July 23/84	3:11	2	0.9/0.9/1.0	
15	July 23/84	3:12	3	1.1/1.5/1.3	
15	July 23/84	3:13	4	1.3/1.2/1.4	Plotted
15	July 23/84	3:22	5	1.3/1.2/1.4	Clamps Loose
51	July 24/84	10:08	1	0.8/0.7/0.8	
51	July 24/84	10:09	2	0.9/09/1.0	
51	July 24/84	10:10	3	1.1/1.5/1.3	
51	July 24/84	10:11	4	1.3/2.2/1.4	Plotted
51	July 24/84	10:12	5	1.3/2.2/1.4	Clamps Loose
35	July 24/84	11:11	1	0.8/0.7/0.8	
35	July 24/84	11:12	2	0.9/0.9/1.0	
35	July 24/84	11:13	3	1.1/1.5/1.3	
35	July 24/84	11:14	4	1.2/1.7/1.2	Plotted
51	Dec 7/84	9:55	1	1.4/1.2/1.6	
51	Dec 7/84	10:00	2	1.9/2.8/2.7	Plotted
23	Dec 7/84	1:40	1	1.4/1.2/1.6	
23	Dec 7/84	1:45	2	1.9/2.2/2.5	Plotted
Rack Test					
23,10,15	July 25/84	2:45	1	0.8/0.7/0.8	
23,10,15	July 25/84	2:46	2	0.9/0.9/1.0	
23,10,15	July 25/84	2:47	3	1.1/1.5/1.3	
23,10,15	July 25/84	2:49	4	1.1/ * /1.1	Plotted

*Signal Distorted - No Reliable Data Available

TABLE 3

SEISMIC TEST RESULTS

CELL NUMBER	DIRECTION	ZPA	FIGURE
Single-Cell Tests - First Stage			
57	X	1.31	3
57	Y	0.98	4
57	Z	1.59	5
15	X	1.26	6
15	Y	1.15	7
15	Z	1.40	8
51	X	1.29	9
51	Y	2.24	10
51	Z	1.40	11
35	X	1.21	12
35	Y	1.71	13
35	Z	1.22	14
Single-Cell Tests - Second Stage			
51	Y	1.9	15
51	Z	2.8	16
51	X	2.7	17
23	X	1.9	18
23	Y	2.2	19
23	Z	2.5	20
Rack Tests			
15,23,10	X	1.13	21
15,23,10	Y	Signal Lost	
15,23,10	Z	1.13	22

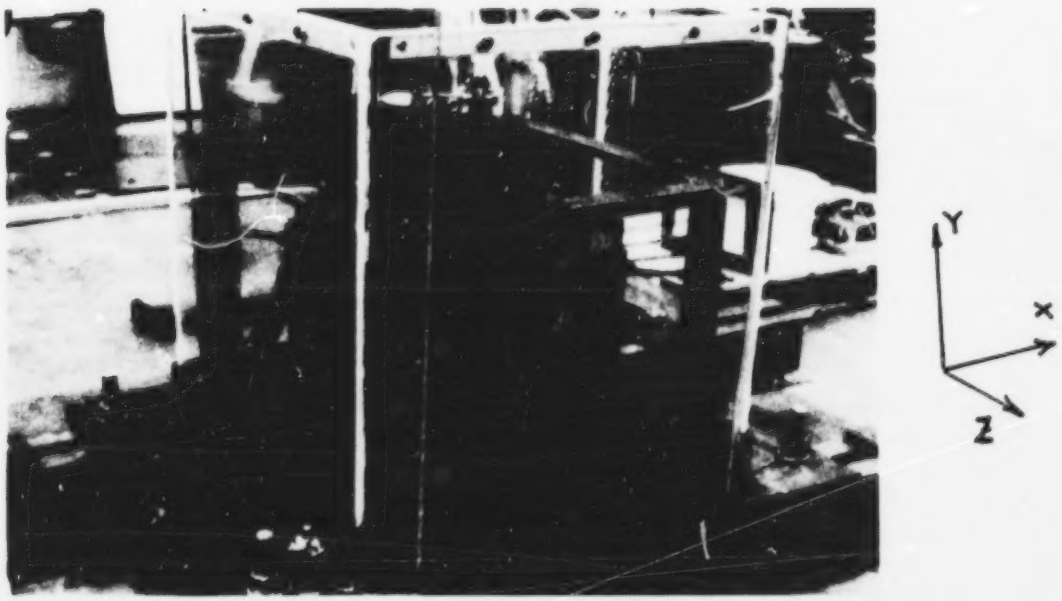


Figure 1

Typical mounting of an Exide FHC-19 cell in single-cell frame. Cell is clamped at four corners with threaded rods. Accelerometers are mounted on the base and on one of the terminal posts.

Axes of vibration are indicated.

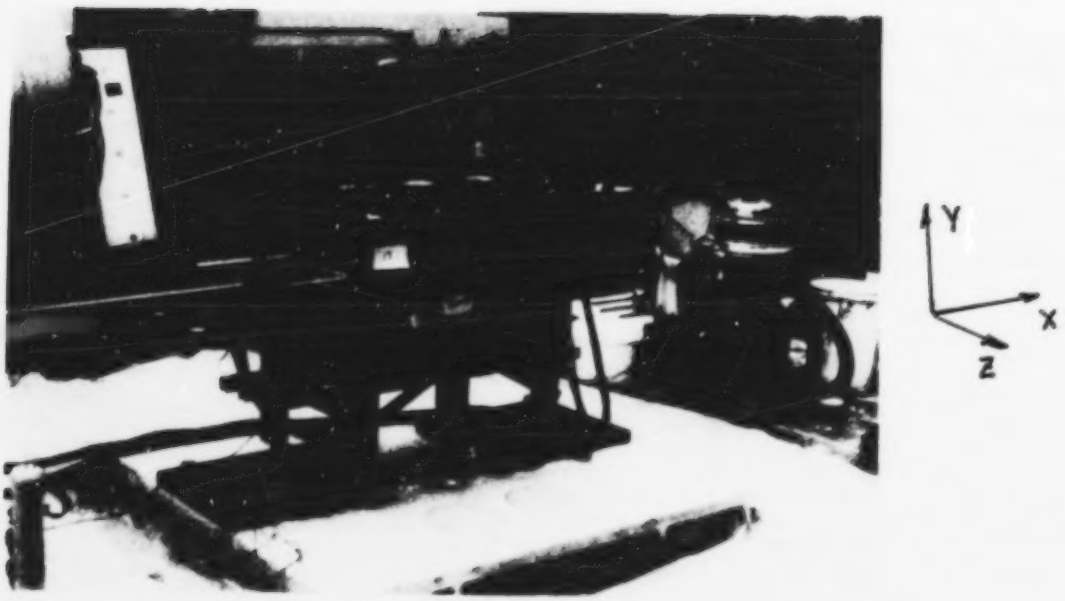
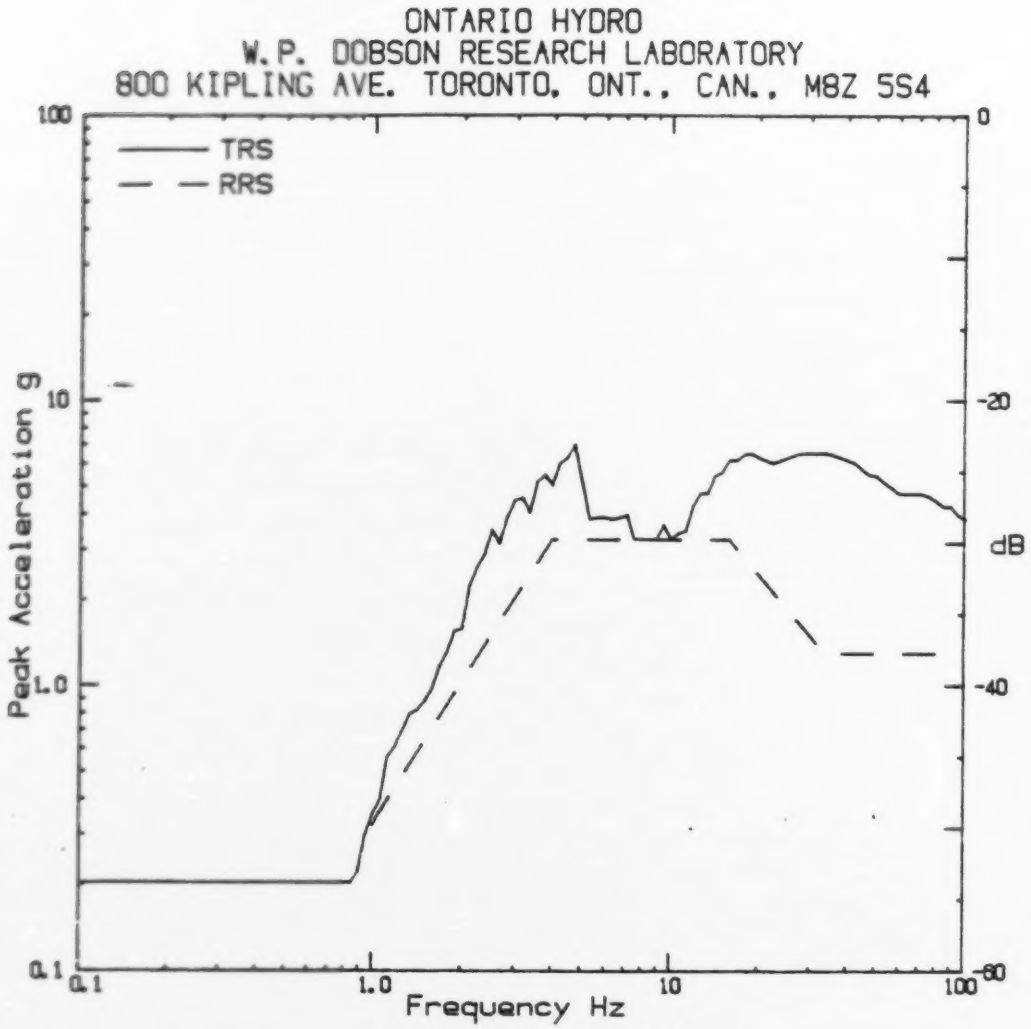


Figure 2

Mounting of Exide FHC-19 cells in multi-cell rack.
Axes of vibration are indicated.



RESPONSE SPECTRUM

FIGURE 3

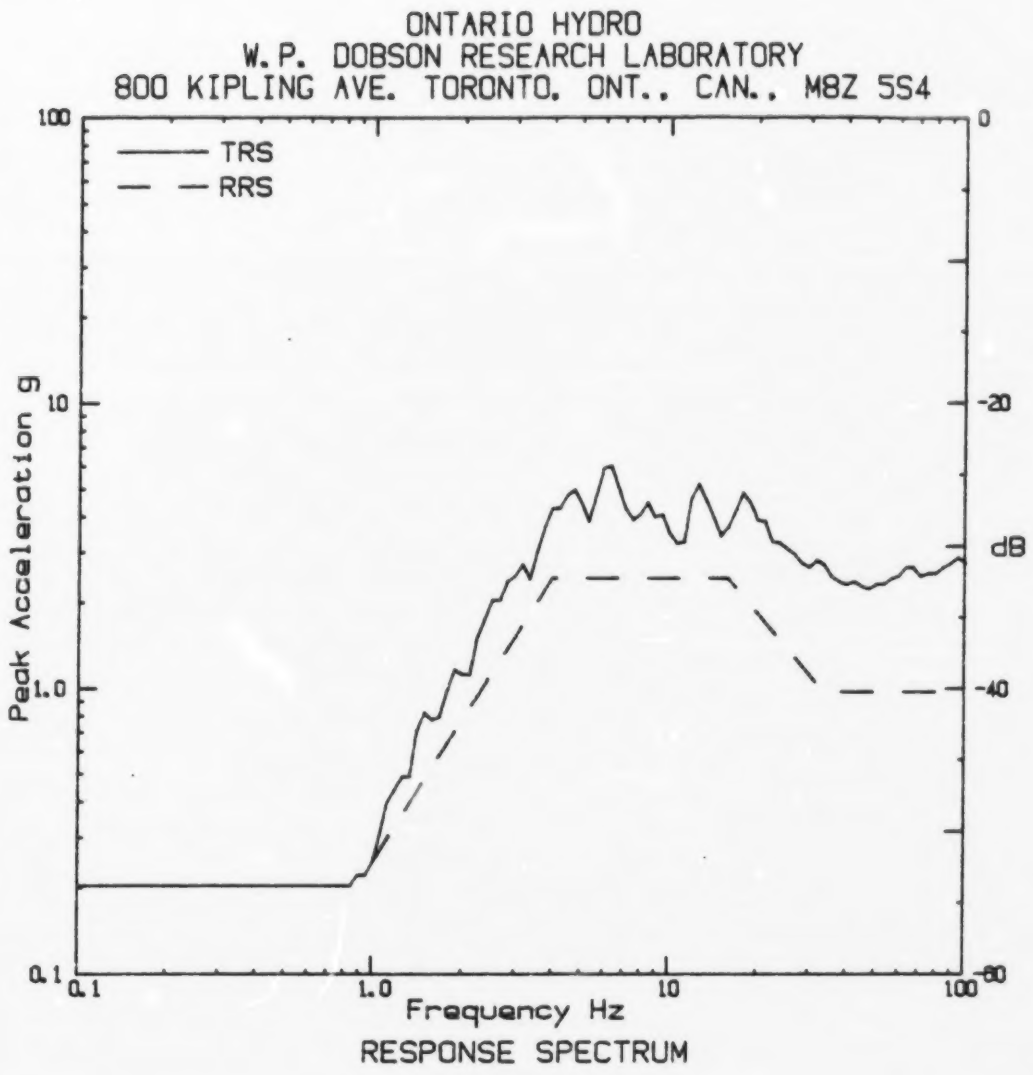
TEST ITEM
Station cell. Exide. Model FHC-19. Serial 57. Calvert Cliffs N.P.P.

PARTICULARS
July 23/84. Time 2:13. Temp('C) 23. Humidity(%) 53. Press (kPa) 100.2.
Graph 5200

SPECIFICATIONS
Specs IEEE 501. Conditions operating. 3 hour rate ; span 7

ANALYSIS
Type Maximax. Damping (%) 5. B.W. = 1/12 Octaves. Axis X.
Shaker tri-axial. ZPA=1.31g

ACCELEROMETER
Wilcoxon. Serial S771. Range dB49. Location base-mounting plate.
Channel 1



RESPONSE SPECTRUM

FIGURE 4

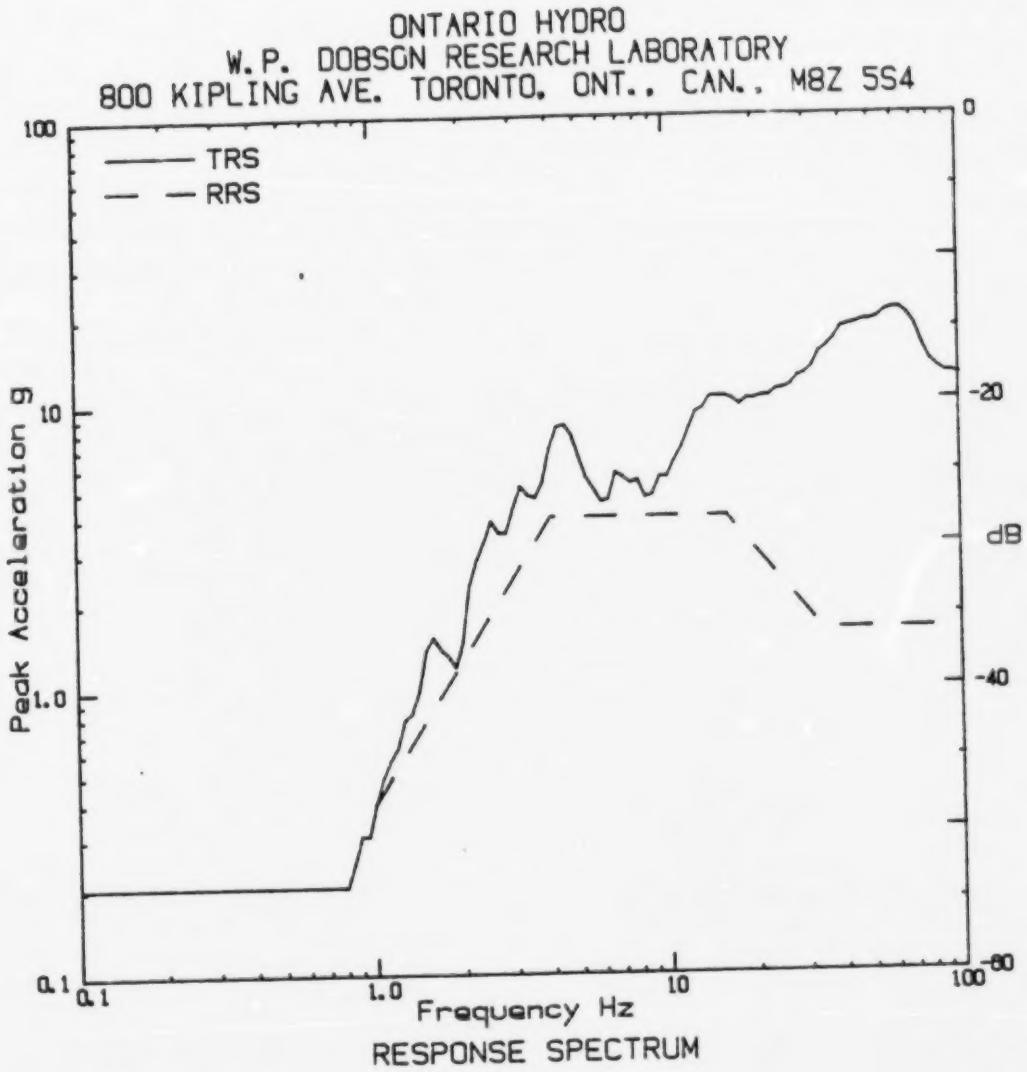
TEST ITEM
Station cell. Exide. Model FHC-19. Serial 57. Calvert Cliffs N.P.P.

PARTICULARS
July 23/84. Time 2:13. Temp('C) 23. Humidity(%) 53. Press (kPa) 100.2.
Graph 5201

SPECIFICATIONS
Specs IEEE 501. Conditions operating. 3 hour rate : span 7

ANALYSIS
Type Maximax. Damping (%) 5. B.W. = 1/12 Octaves. Axis Y.
Shaker tri-axial. ZPA=.98g

ACCELEROMETER
Wilcoxon. Serial S761. Range dB49. Location base-mounting plate.
Channel 2



RESPONSE SPECTRUM

FIGURE 5

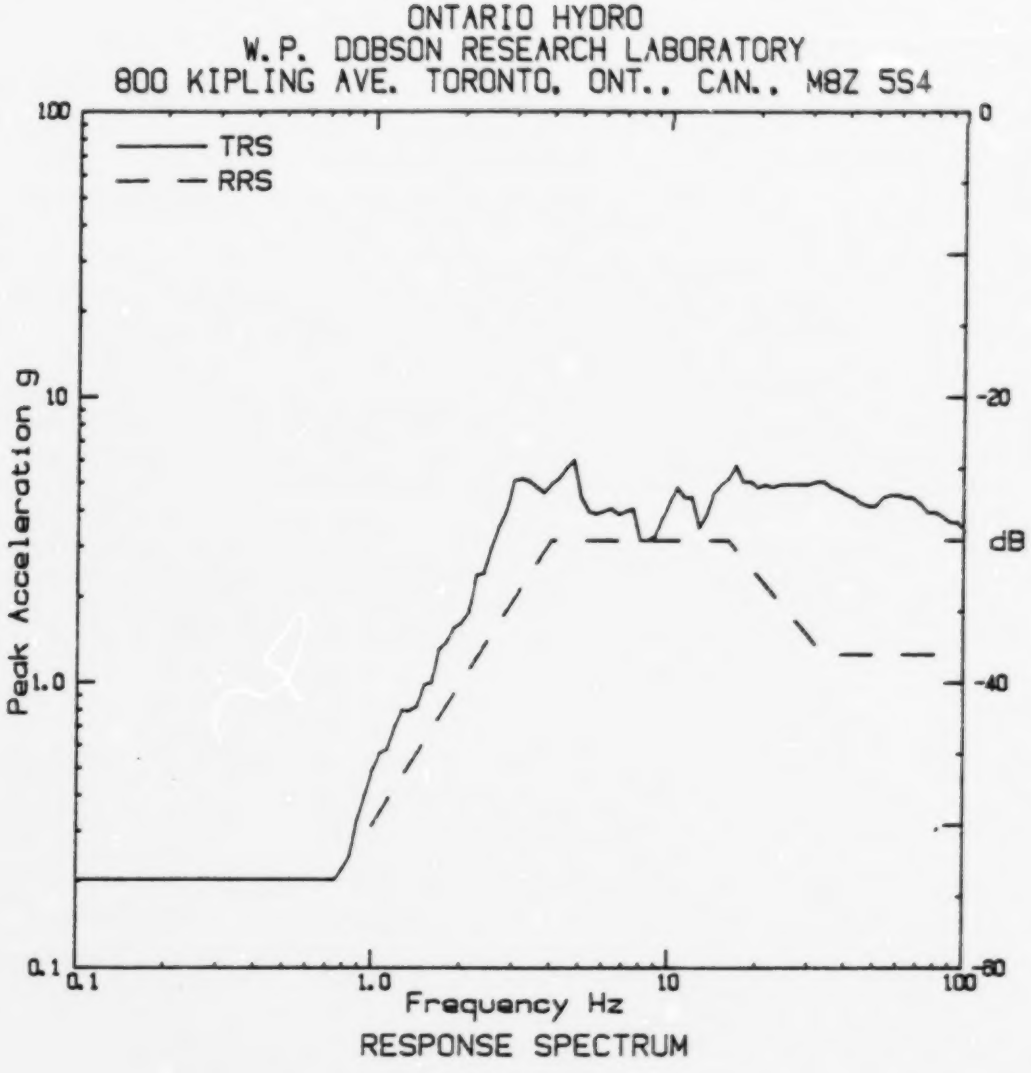
TEST ITEM
Station cell. Exide. Model FHC-19. Serial 57. Calvert Cliffs N.P.P.

PARTICULARS
July 23/84. Time 2:13. Temp('C) 23. Humidity(%) 53. Press (kPa) 100.2.
Graph 5202

SPECIFICATIONS
Specs IEEE 501. Conditions operating. 3 hour rate : span 7

ANALYSIS
Type Maximax. Damping (%) 5. B.W. = 1/12 Octaves. Axis Z.
Shaker tri-axial. ZPA=1.59g

ACCELEROMETER
Wilcoxon. Serial S297. Range dB49. Location base-mounting plate.
Channel 3



RESPONSE SPECTRUM

FIGURE 6

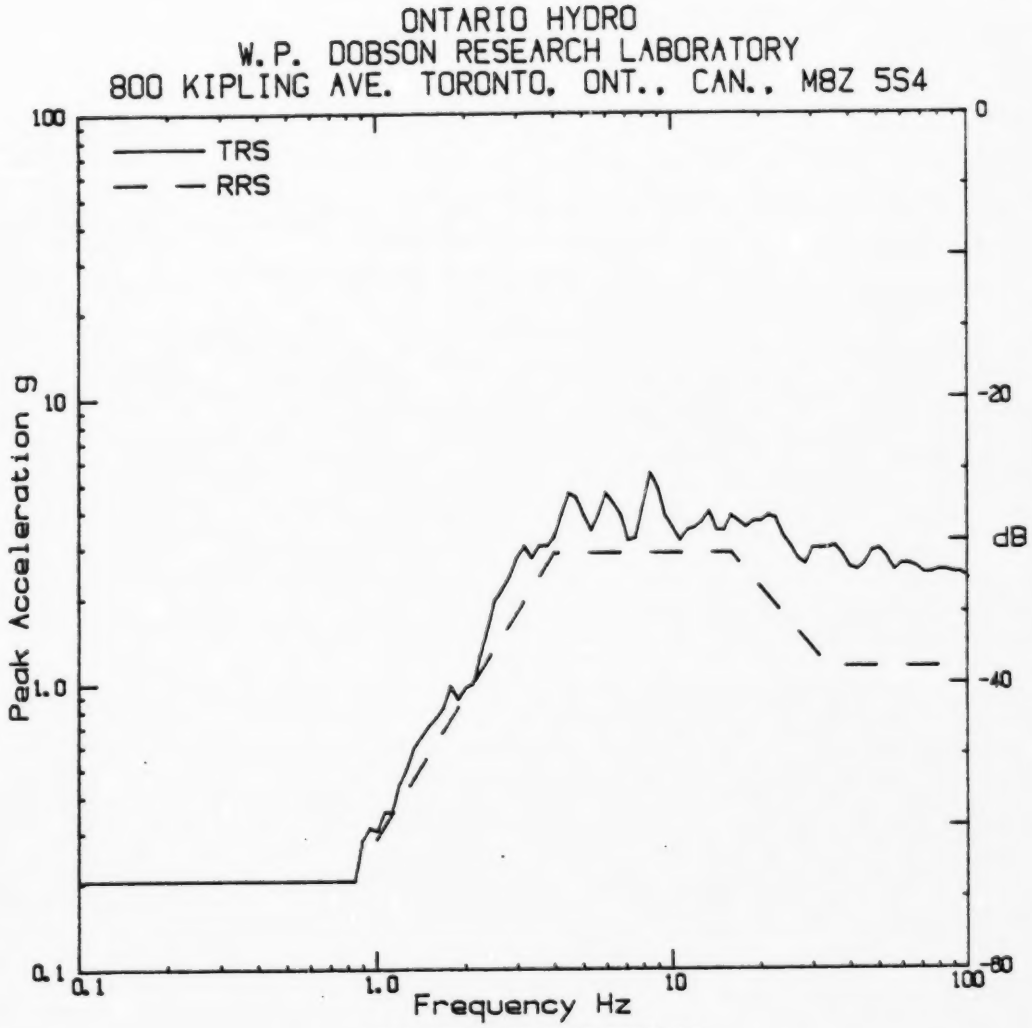
TEST ITEM
Station cell, Exide, Model FHC-19, Serial 15, Calvert Cliffs N.P.P.

PARTICULARS
July 23/84, Time 2:45, Temp('C) 23, Humidity(%) 53, Press (kPa) 100.2,
Graph 5206

SPECIFICATIONS
Specs IEEE 501, Conditions operating ; 3 hour rate, span 7

ANALYSIS
Type Maximax, Damping (%) 5, B.W. = 1/12 Octaves, Axis X,
Shaker tri-axial, ZPA=1.26g

ACCELEROMETER
Wilcoxon, Serial S771, Range d849, Location base-mounting plate,
Channel 1



RESPONSE SPECTRUM

FIGURE 7

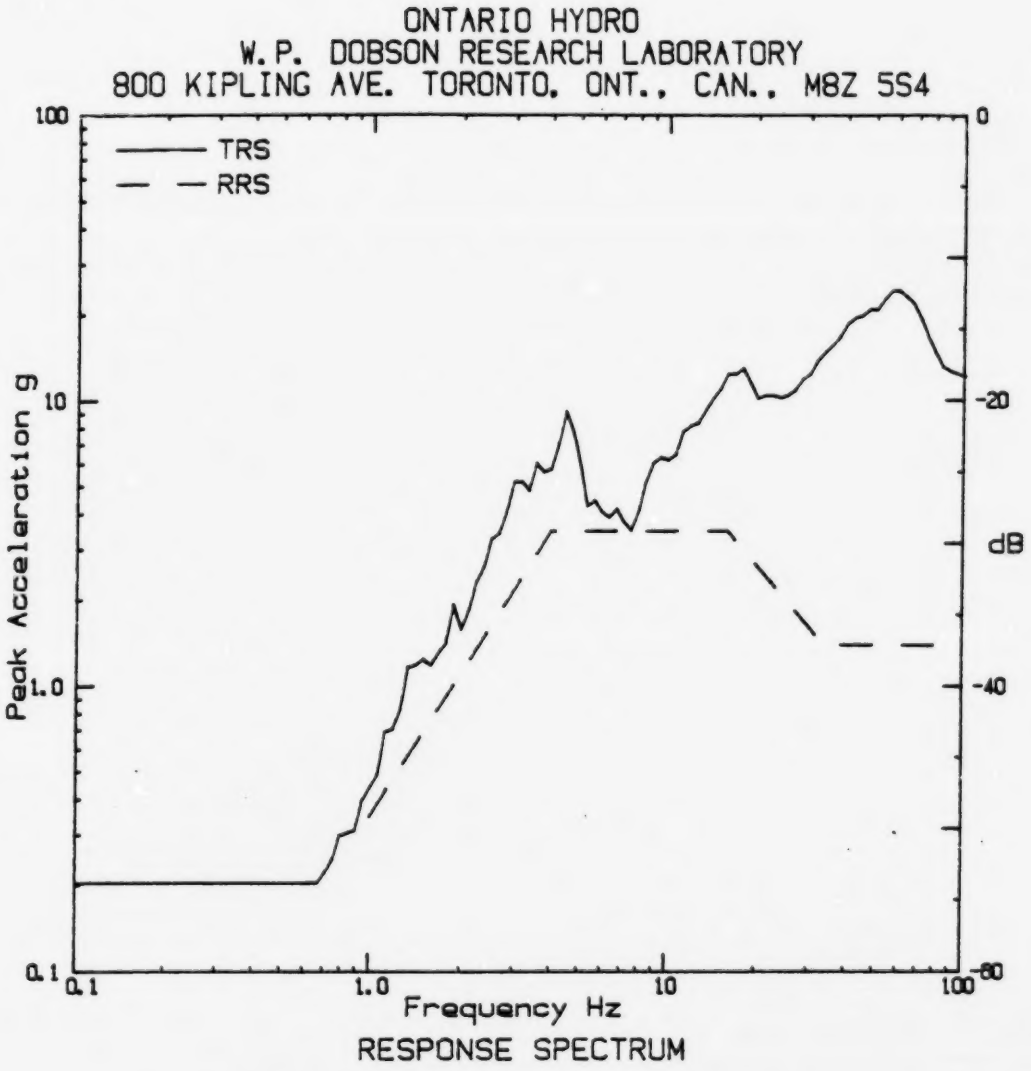
TEST ITEM
Station cell. Exide. Model FHC-19. Serial 15. Calvert Cliffs N.P.P.

PARTICULARS
July 23/84. Time 2:45. Temp('C) 23. Humidity(%) 53. Press (kPa) 100.2.
Graph 5207

SPECIFICATIONS
Spece IEEE 501. Conditions operating : 3 hour rate. span 7

ANALYSIS
Type Maximax. Damping (%) 5. B.W. = 1/12 Octaves. Axis Y.
Shaker tri-axial. ZPA=1.15g

ACCELEROMETER
Wilcoxon. Serial S761. Range dB49. Location base-mounting plate.
Channel 2



RESPONSE SPECTRUM

FIGURE 8

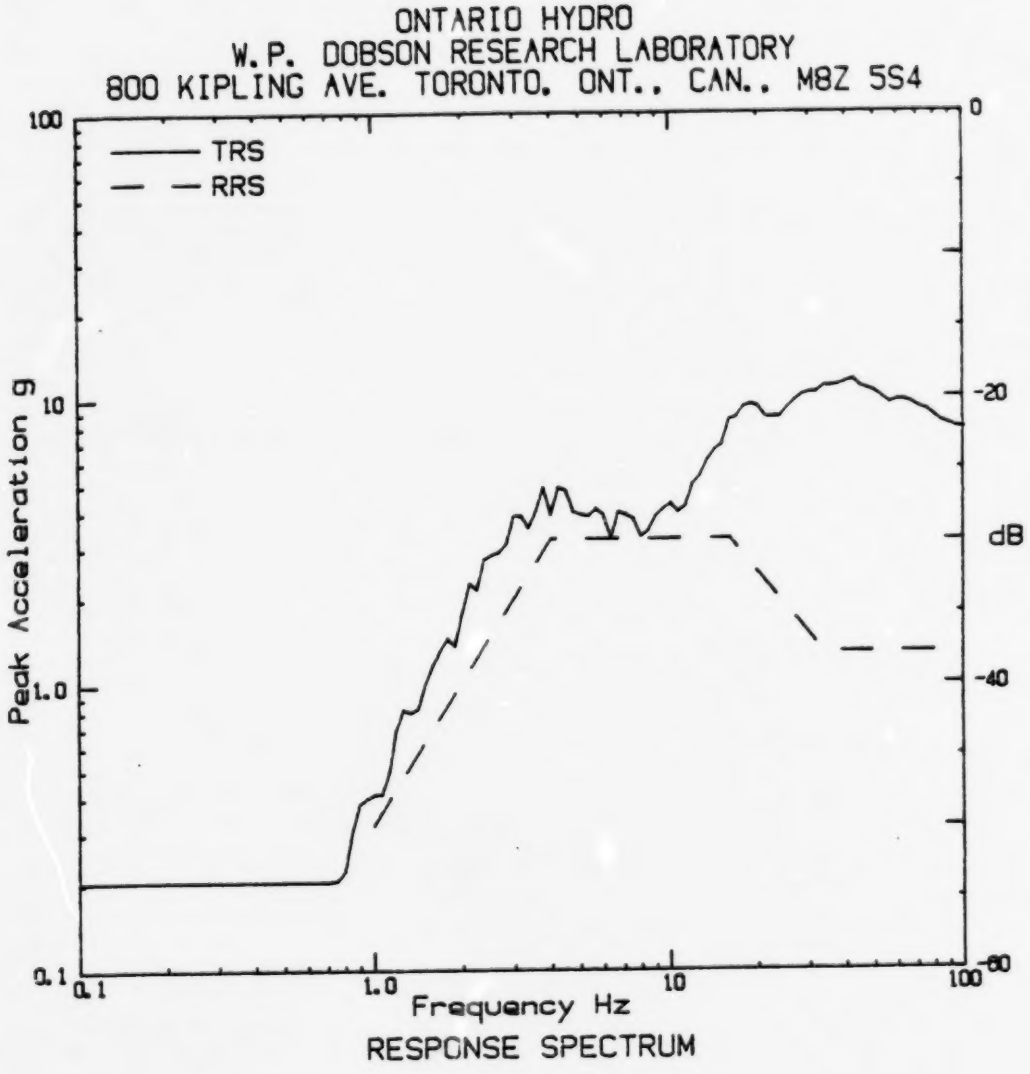
TEST ITEM
Station call. Exide. Model FHC-19. Serial 15. Calvert Cliffs N.P.P.

PARTICULARS
July 23/84. Time 2:45. Temp('C) 23. Humidity(%) 53. Press (kPa) 100.2.
Graph 5208

SPECIFICATIONS
Spec IEEE 501. Conditions operating ; 3 hour rate. span 7

ANALYSIS
Type Maximax. Damping (%) 5. B.W. = 1/12 Octaves. Axis Z.
Shaker tri-axial. ZPA=1.4g

ACCELEROMETER
Wilcoxon. Serial S297. Range dB49. Location base-mounting plate.
Channel 3



RESPONSE SPECTRUM

FIGURE 9

TEST ITEM
Station cell. Exide. Model FHC-19. Serial 51. Calvert Cliffs N.P.P.

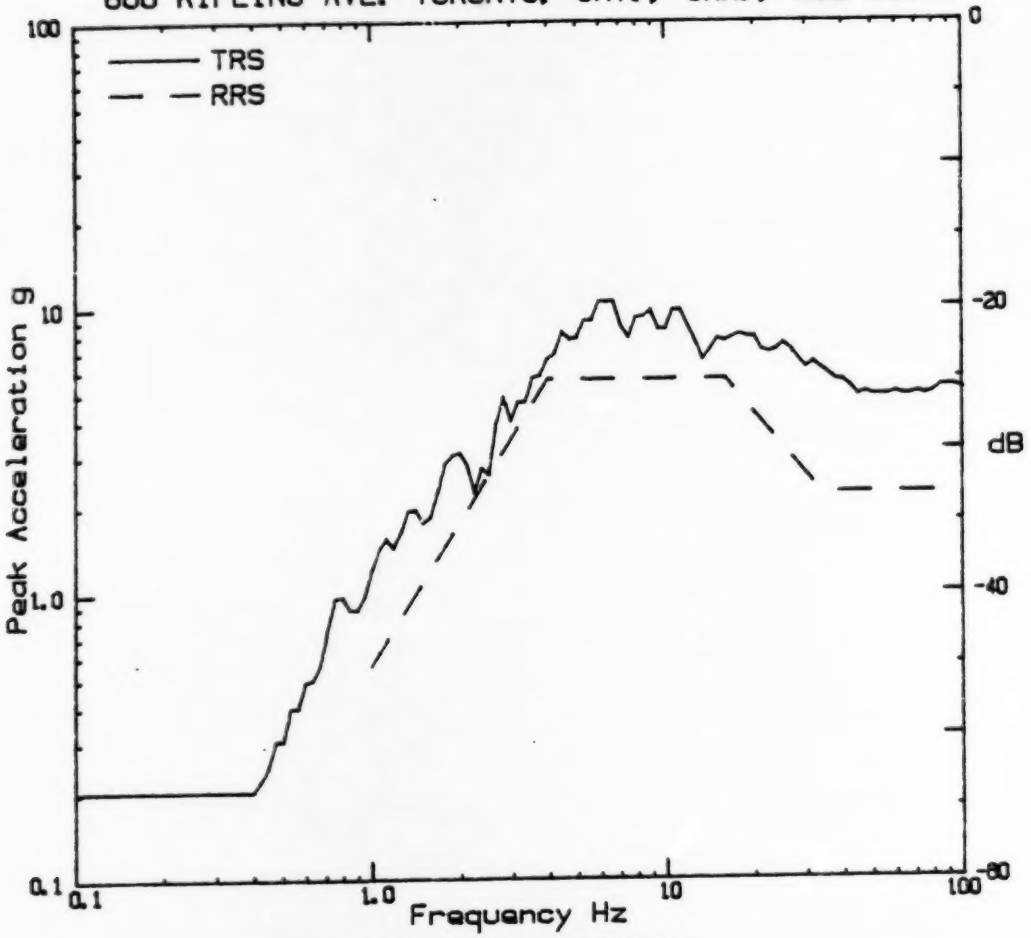
PARTICULARS
July 23/84. Time 10:12. Temp('C) 23. Humidity(%) 53.
Press (kPa) 100.2. Graph 5212

SPECIFICATIONS
Specs IEEE 501. Conditions operating : 3 hour rate. span 7

ANALYSIS
Type Maximax. Damping (%) 5. B.W. = 1/12 Octaves. Axis X.
Shaker tri-axial. ZPA=1.29g

ACCELEROMETER
Wilcoxon. Serial S771. Range dB49. Location base-mounting plate.
Channel 1

ONTARIO HYDRO
W.P. DOBSON RESEARCH LABORATORY
800 KIPLING AVE. TORONTO, ONT., CAN., M8Z 5S4



RESPONSE SPECTRUM

FIGURE 10

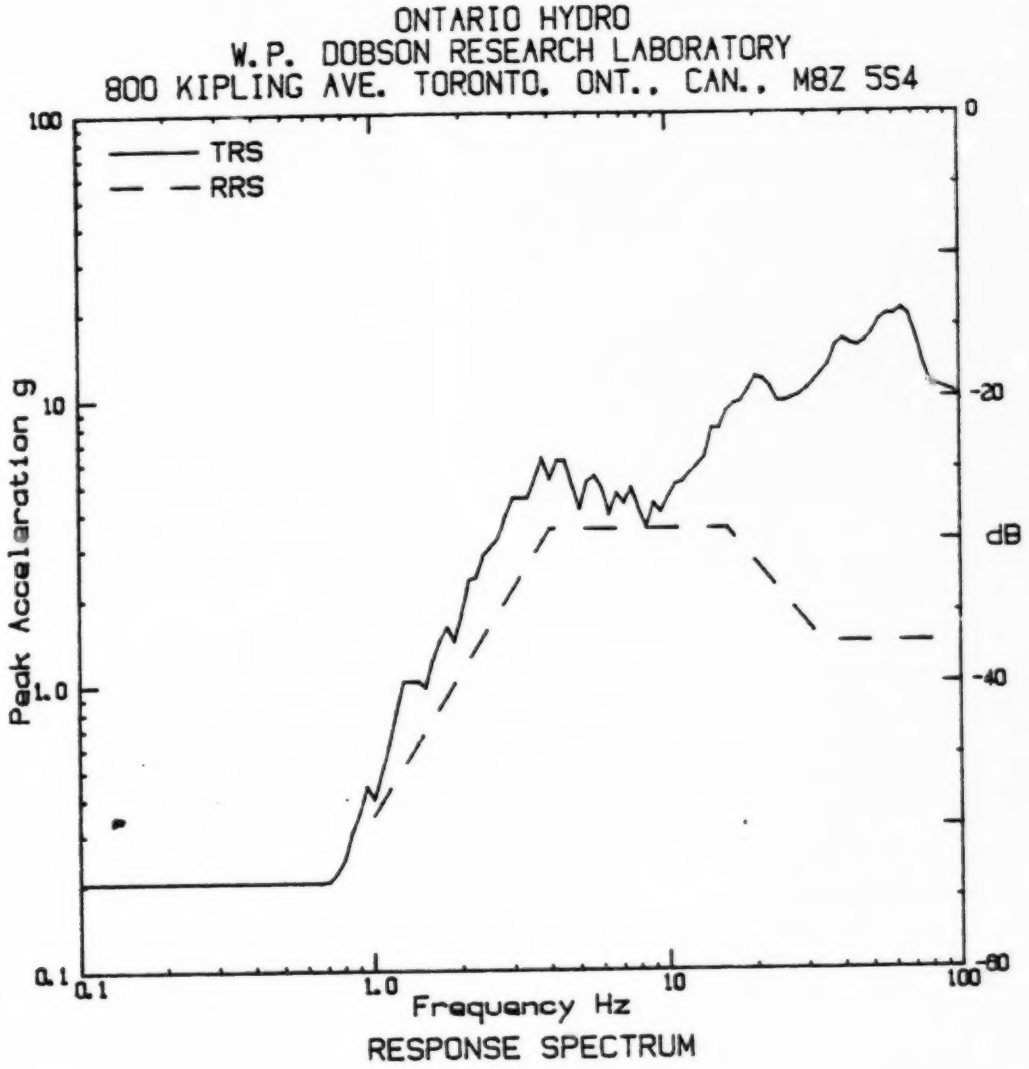
TEST ITEM
Station cell. Exide. Model FHC-19. Serial 51. Calvert Cliffs N.P.P.

PARTICULARS
July 23/84. Time 10:12. Temp(°C) 23. Humidity(%) 53.
Press (kPa) 100.2. Graph 5213

SPECIFICATIONS
Spec IEEE 501. Conditions operating ; 3 hour rate. span 7

ANALYSIS
Type Maximax. Damping (%) 5. B.W. = 1/12 Octaves. Axis Y.
Shaker tri-axial. ZPA=2.24g

ACCELEROMETER
Wilcoxon. Serial S761. Range dB49. Location base-mounting plate.
Channel 2



RESPONSE SPECTRUM

FIGURE 11

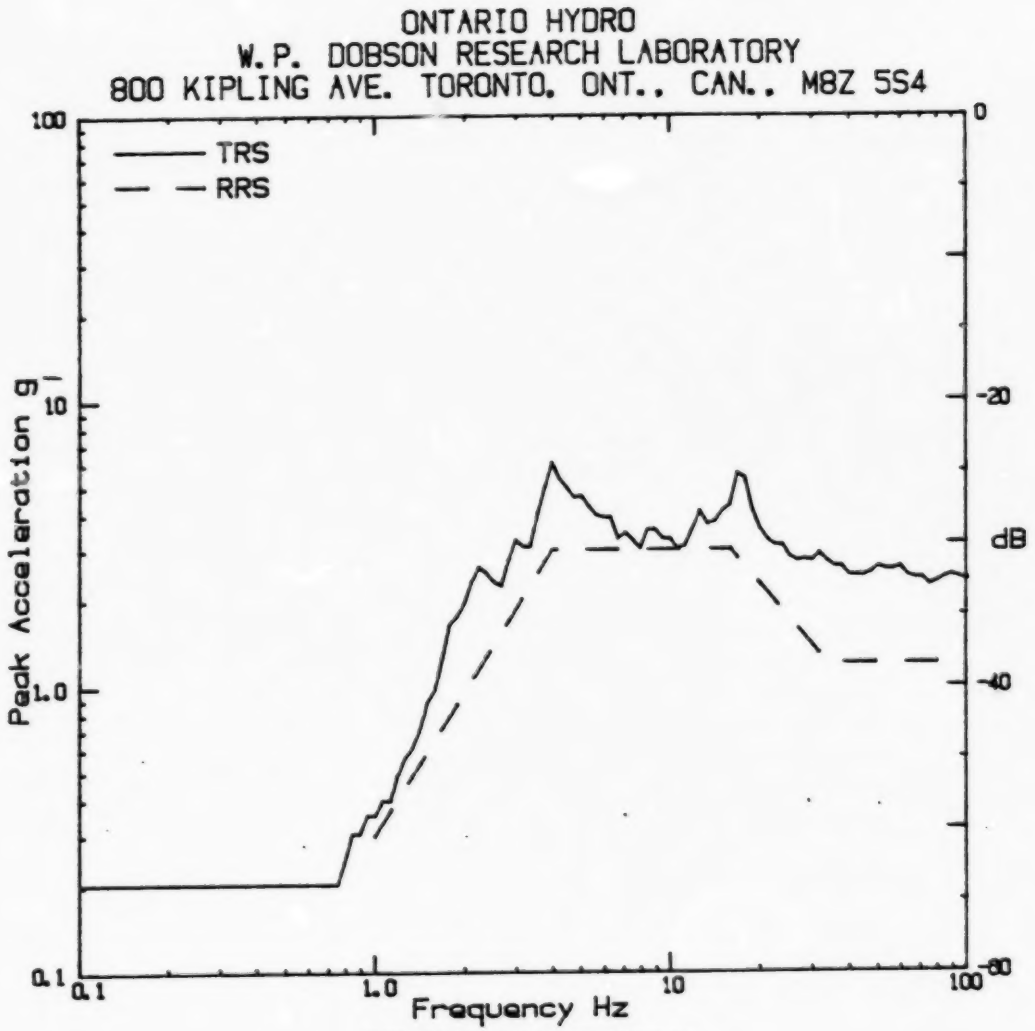
TEST ITEM
Station cell. Exide. Model FHC-19. Serial 51. Calvert Cliffs N.P.P.

PARTICULARS
July 23/84. Time 10:12. Temp('C) 23. Humidity(%) 53.
Press (kPa) 100.2. Graph 5214

SPECIFICATIONS
Spec: IEEE 501. Conditions operating ; 3 hour rate. span 7

ANALYSIS
Type Maximax. Damping (%) 5. B.W. = 1/12 Octaves. Axis Z.
Shaker tri-axial. ZPA=1.4g

ACCELEROMETER
Wilcoxon. Serial S297. Range dB49. Location base-mounting plate.
Channel 3



RESPONSE SPECTRUM

FIGURE 12

TEST ITEM
Station cell. Exide. Model FHC-19. Serial 35. Calvert Cliffs N.P.P.

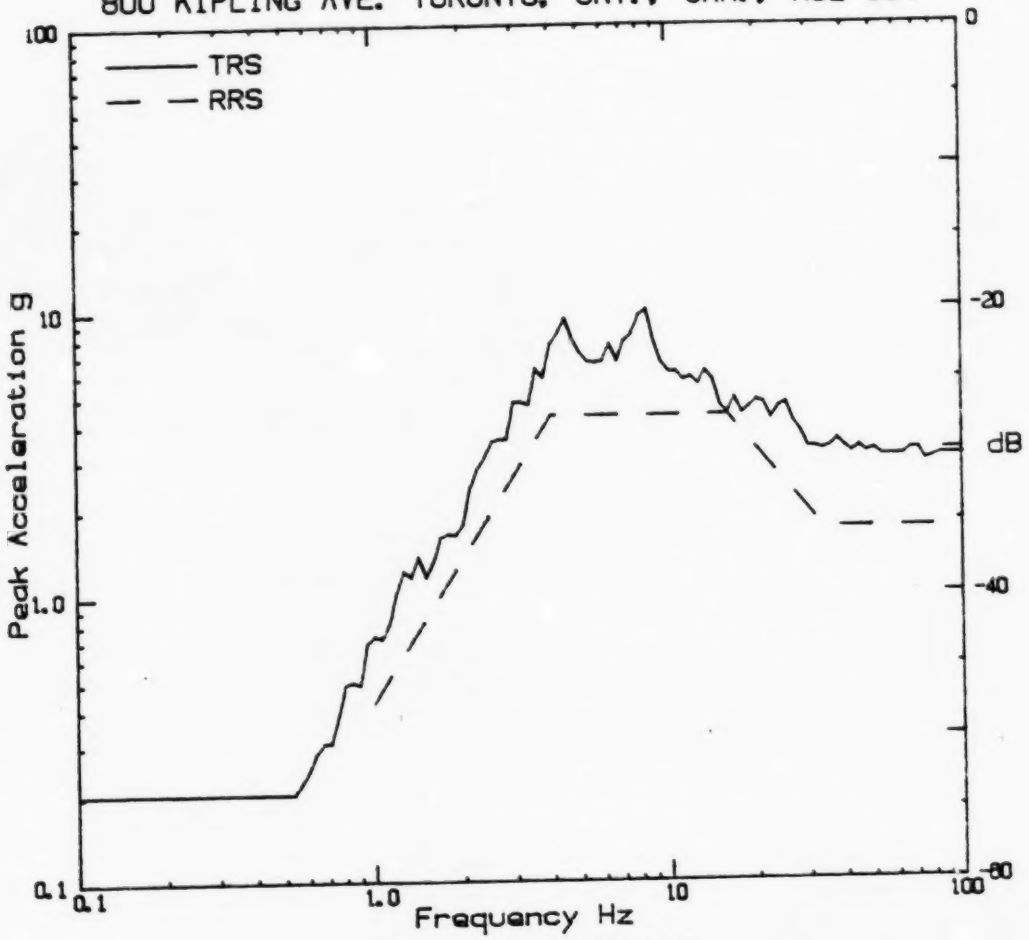
PARTICULARS
July 23/84. Time 11:14. Temp('C) 23. Humidity(%) 53.
Press (kPa) 100.2. Graph 5218

SPECIFICATIONS
Spec: IEEE 501. Conditions operating ; 3 hour rate. span 7

ANALYSIS
Type Maximax. Damping (%) 5. B.W. = 1/12 Octaves. Axis X.
Shaker tri-axial. ZPA=1.21g

ACCELEROMETER
Wilcoxon. Serial S771. Range dB49. Location base-mounting plate.
Channel 1

ONTARIO HYDRO
W.P. DOBSON RESEARCH LABORATORY
800 KIPLING AVE. TORONTO, ONT., CAN., M8Z 5S4



RESPONSE SPECTRUM

FIGURE 13

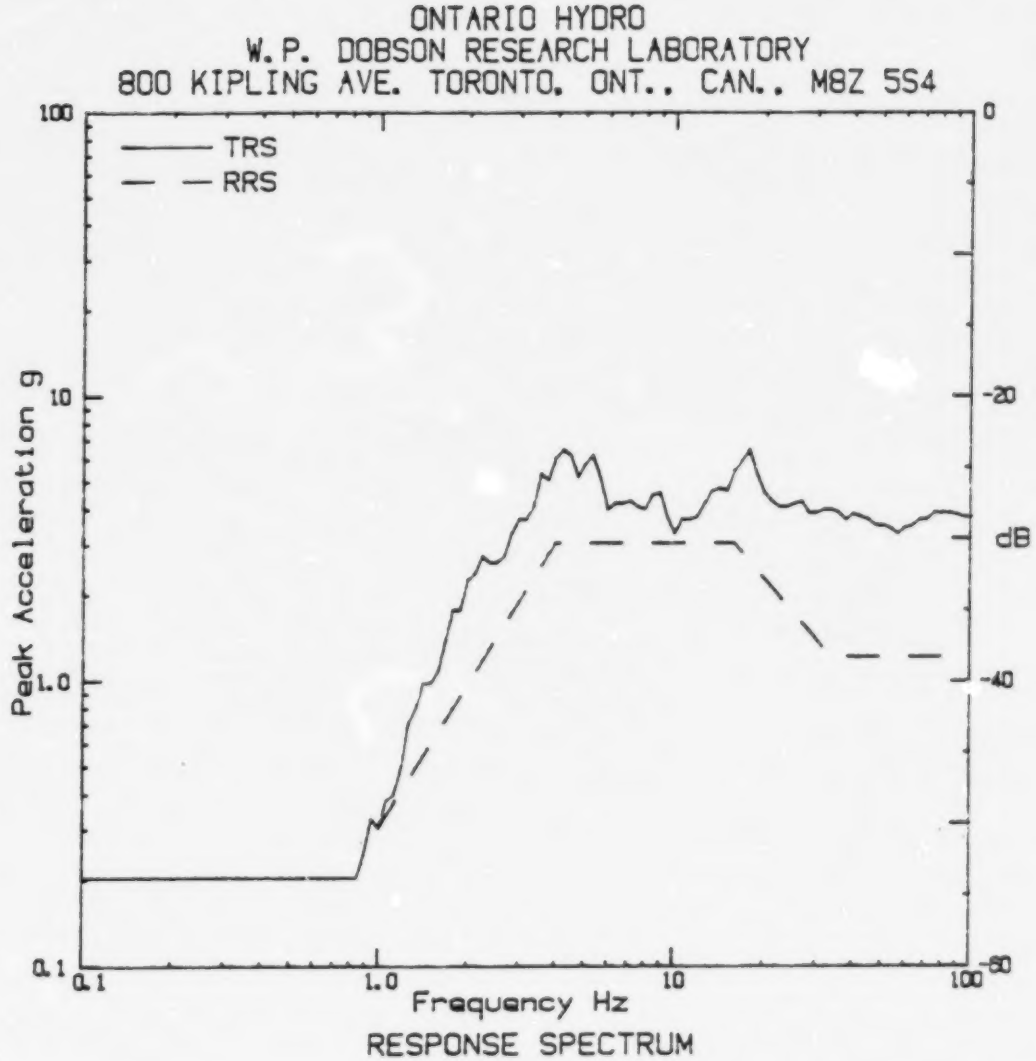
TEST ITEM
Station cell. Exide. Model FHC-19. Serial 35. Calvert Cliffs N.P.P.

PARTICULARS
July 23/84. Time 11:14. Temp('C) 23. Humidity(%) 53.
Press (kPa) 100.2. Graph 5219

SPECIFICATIONS
Specs IEEE 501. Conditions operating : 3 hour rate. span 7

ANALYSIS
Type Maximax. Damping (%) 5. B.W. = 1/12 Octaves. Axis Y.
Shaker tri-axial. ZPA=1.71g

ACCELEROMETER
Wilcoxon. Serial S761. Range dB49. Location base-mounting plate.
Channel 2



RESPONSE SPECTRUM

FIGURE 14

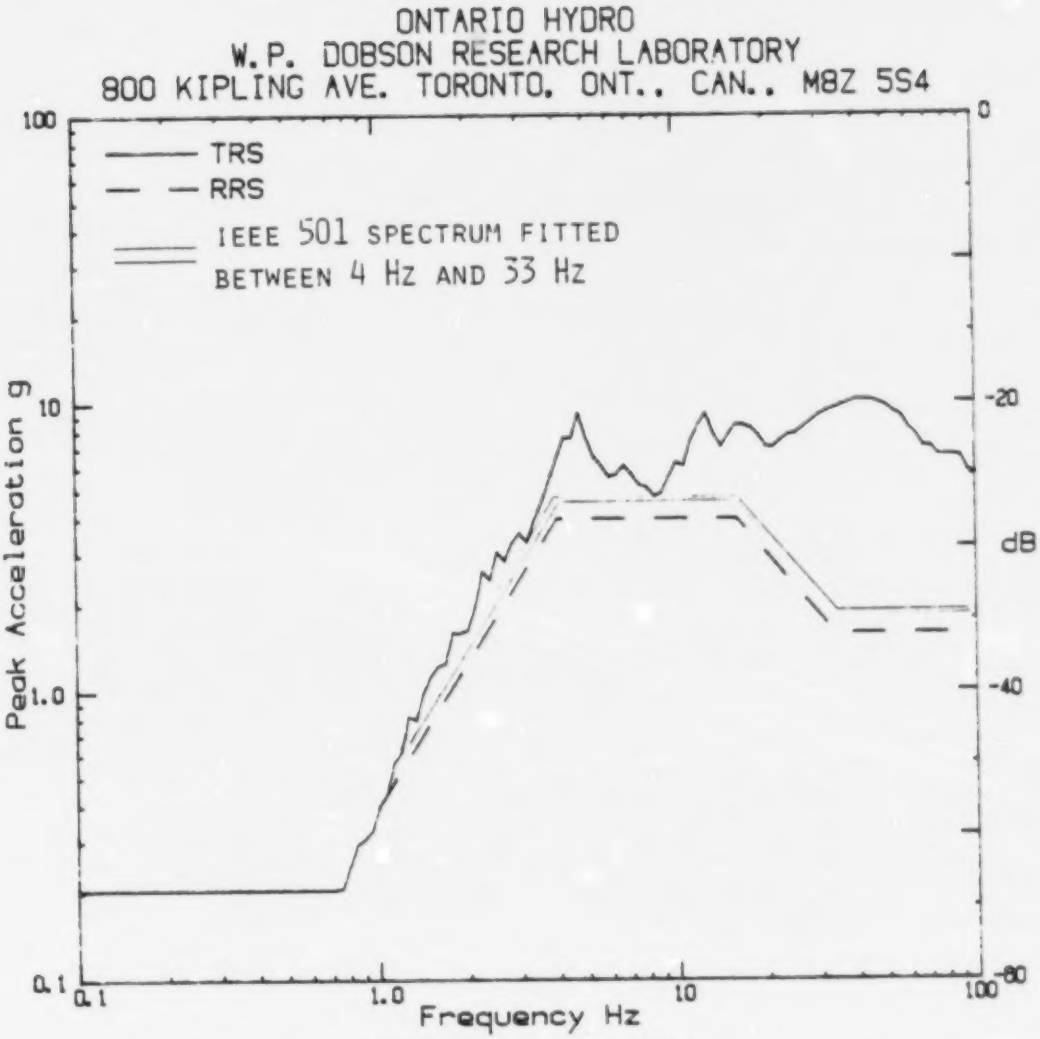
TEST ITEM
station cell, Exide, Model FHC-19, Serial 35, Calvert Cliffs N.P.P.

PARTICULARS
July 23/84, Time 11:14, Temp(°C) 23, Humidity(%) 53.
Press (kPa) 100.2, Graph 5220

SPECIFICATIONS
Specs IEEE 501, Conditions operating ; 3 hour rate, span 7

ANALYSIS
Type Maximax, Damping (%) 5, B.W. = 1/12 Octaves, Axis Z.
Shaker tri-axial, ZPA=1.22g

ACCELEROMETER
Wilcoxon, Serial S297, Range dB49, Location base-mounting plate.
Channel 3



RESPONSE SPECTRUM

FIGURE 15

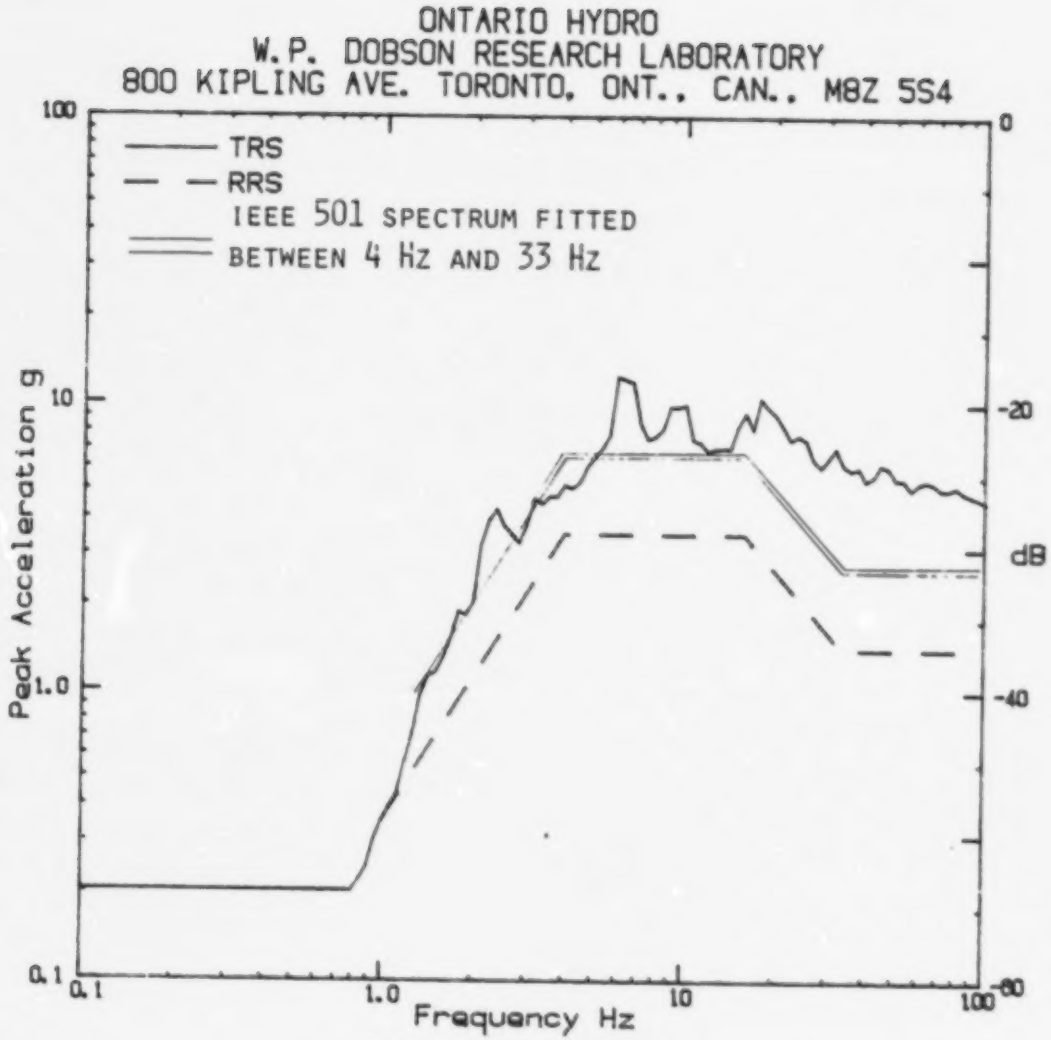
TEST ITEM
Station Cell. Exide. Model FHC 19. Cell #51

PARTICULARS
Dec. 7/84. Time 10:00. Temp('C) 24. Humidity(%) 29. Press (kPa) 100.5.
Graph 5409. Record 0

SPECIFICATIONS
Spec IEEE 344. Conditions operating. table limit

ANALYSIS
Type Maximax. Damping (%) 5. B.W. = 1/12 Octaves. Axis X-base.
Shaker tri-axial. ZPA=1.9 g

ACCELEROMETER
Wilcoxon. Serial 1214. Range dB48. Location muonting plate. TT 722.
Channel 1



RESPONSE SPECTRUM

FIGURE 16

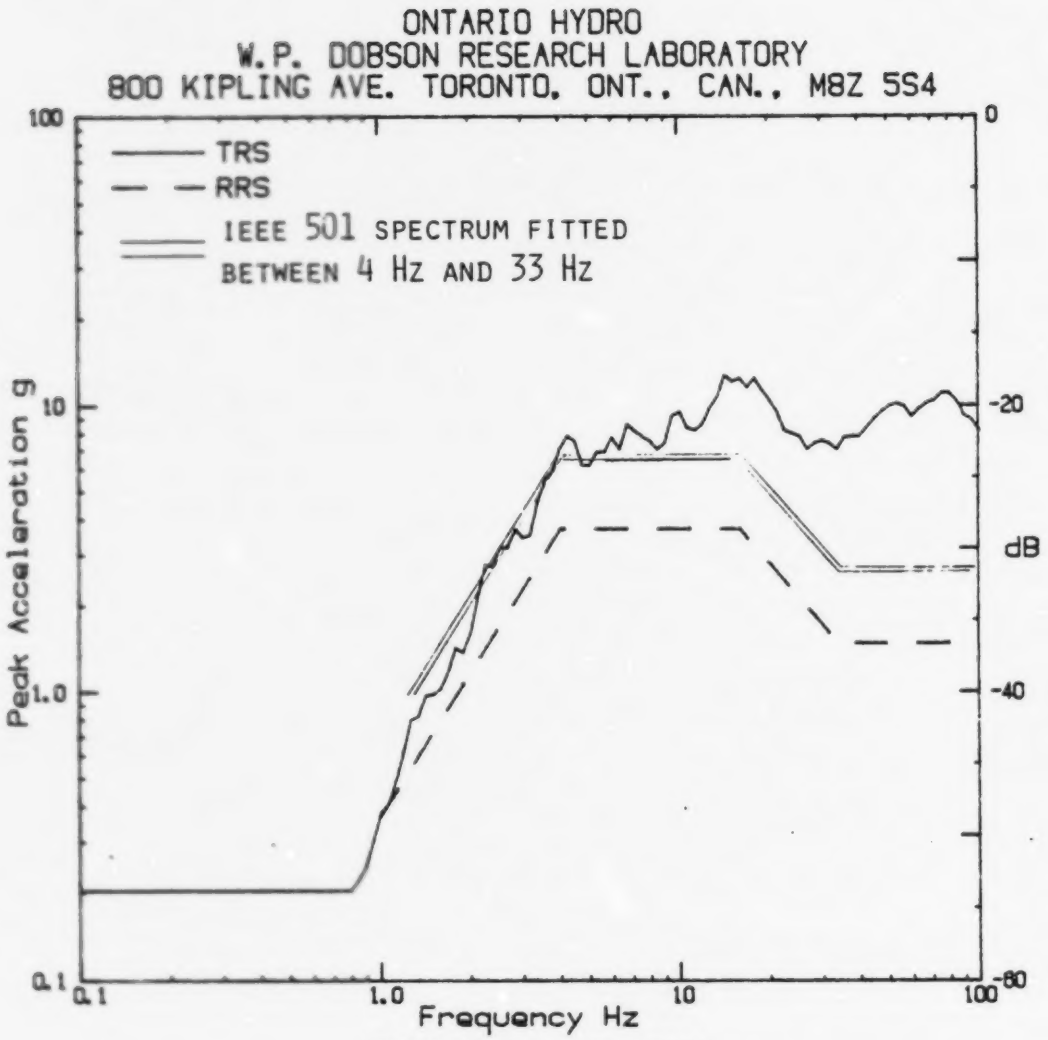
TEST ITEM
Station Cell, Exide, Model FHC 19, Cell #51

PARTICULARS
Dec. 7/84, Time 10:00, Temp('C) 24, Humidity(%) 29, Press (kPa) 100.5, Graph 5410, Record 0

SPECIFICATIONS
Spec: IEEE 344, Conditions operating, table limit

ANALYSIS
Type Maximax, Damping (%) 5, B.W. = 1/12 Octaves, Axis Y-base, Shaker tri-axial, ZPA = 2·8 g

ACCELEROMETER
Wilcoxon, Serial 1215, Range dB48, Location mounting plate, TT 722, Channel 2



RESPONSE SPECTRUM

FIGURE 17

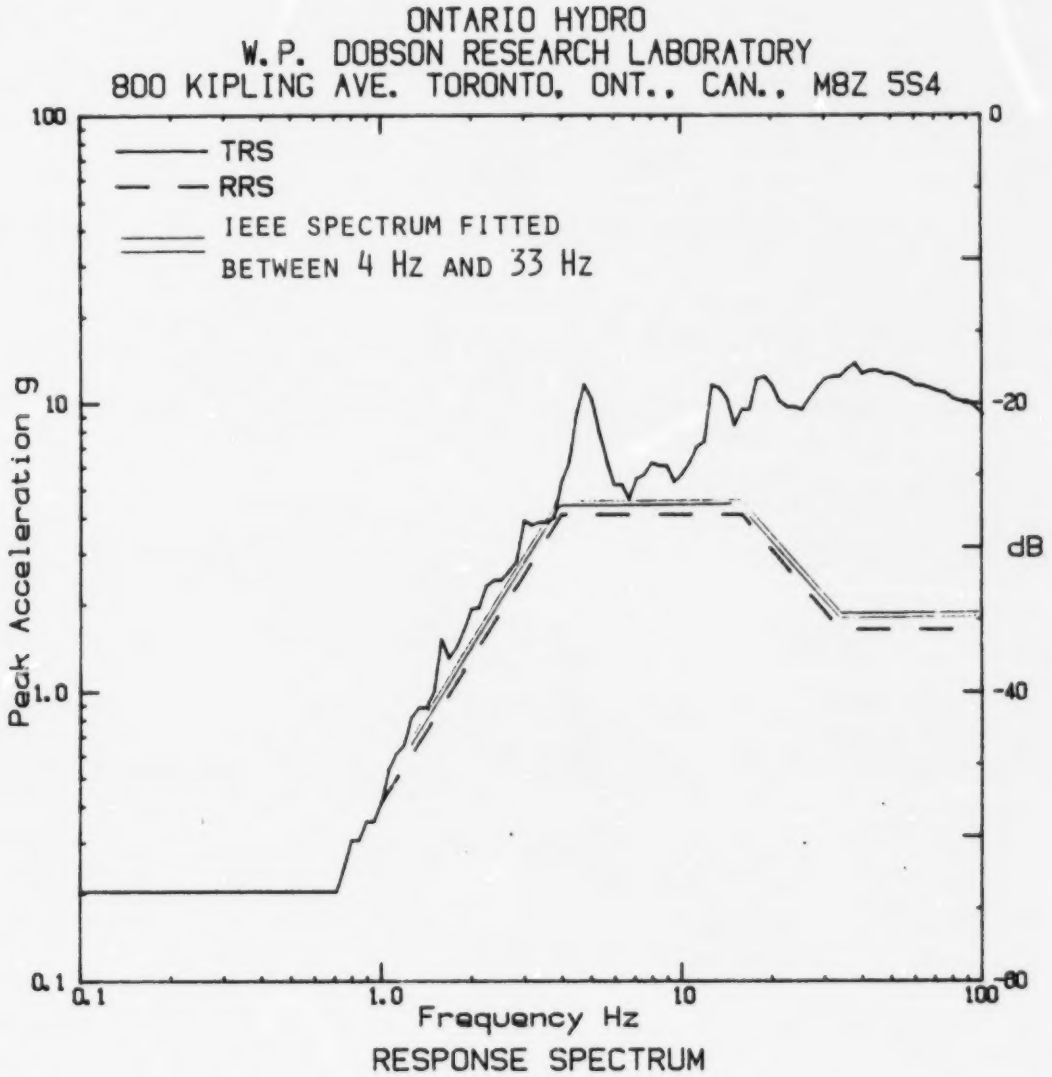
TEST ITEM
Station Cell. Exide. Model FHC 19. Cell #51

PARTICULARS
Dec. 7/84. Time 10:00. Temp('C) 24. Humidity(%) 29. Press (kPa) 100.5.
Graph 5411. Record 0

SPECIFICATIONS
Spece IEEE 344. Conditions operating. table limit

ANALYSIS
Type Maximax. Damping (%) 5. B.W. = 1/12 Octaves. Axis Z-base.
Shaker tri-axial. ZPA = 2.7 g

ACCELEROMETER
Wilcoxon. Serial 1213. Range dB48. Location muonting plate. TT 722.
Channel 3



RESPONSE SPECTRUM

FIGURE 18

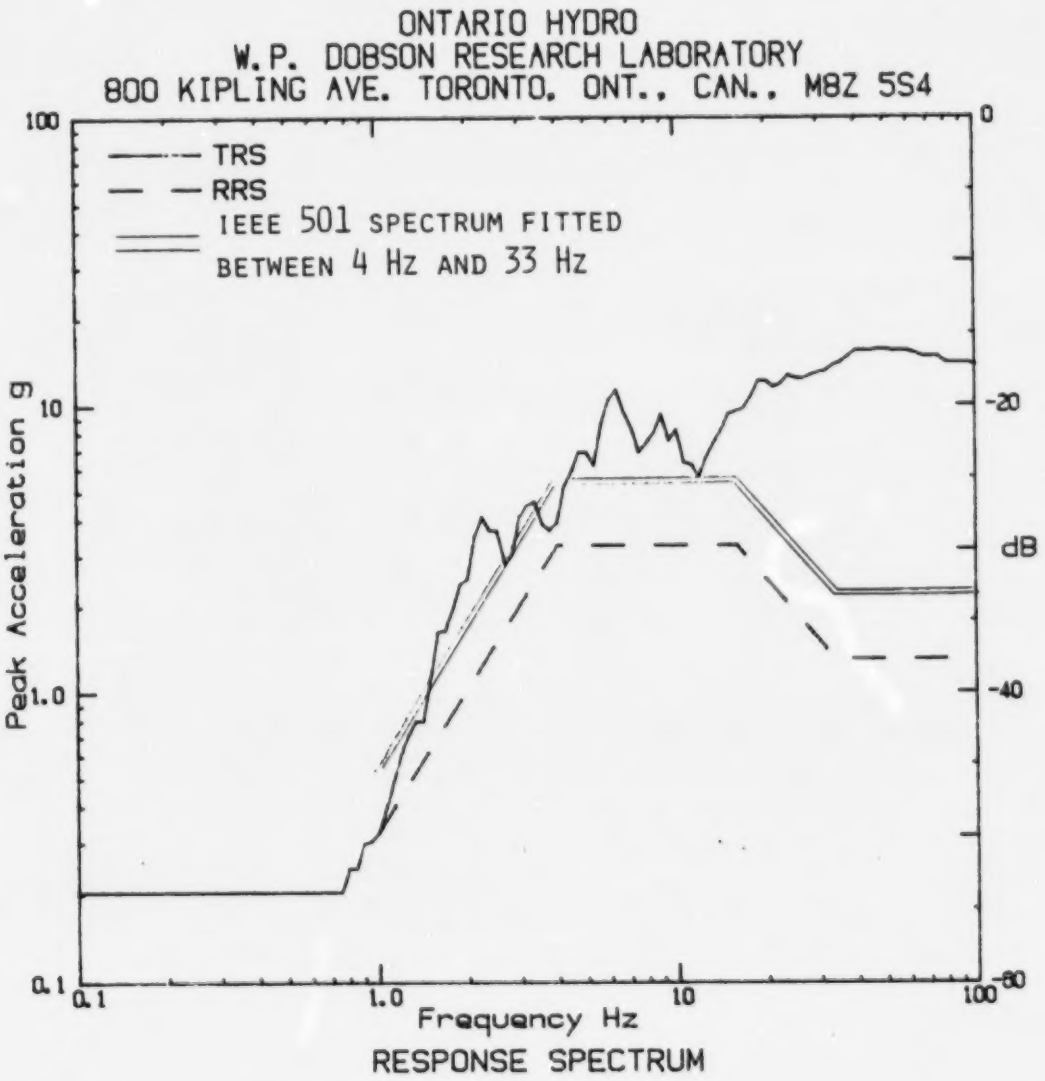
TEST ITEM
Station Cell, Exide, Model FHC 19, Cell #23

PARTICULARS
Dec. 7/84, Time 1:45, Temp('C) 24, Humidity(%) 29, Press (kPa)100.5,
Graph 5415, Record 0

SPECIFICATIONS
Spec: IEEE 344, Conditions operating, table limit

ANALYSIS
Type Maximax, Damping (%)5, B.W. = 1/12 Octaves, Axis X-base,
Shaker tri-axial, ZPA=1.9 g

ACCELEROMETER
Wilcoxon, Serial 1214, Range dB48, Location cell terminal, TT 726,
Channel 1



RESPONSE SPECTRUM

FIGURE 19

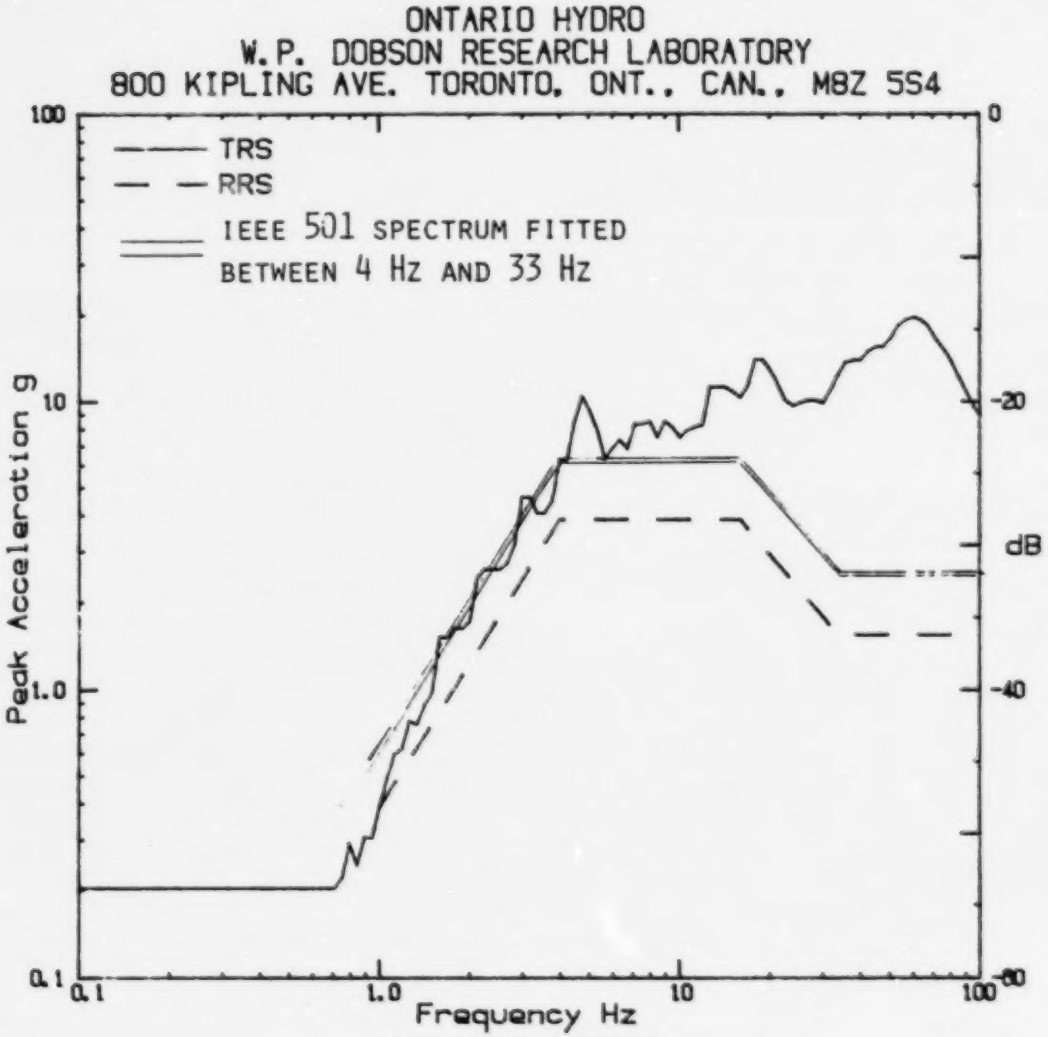
TEST ITEM
Station Cell, Exide, Model FHC 19, Cell #23

PARTICULARS
Dec. 7/84, Time 1:45, Temp('C) 24, Humidity(%) 29, Press (kPa) 100.5, Graph 5416, Record 0

SPECIFICATIONS
Spec: IEEE 344, Conditions operating, table limit

ANALYSIS
Type Maximax, Damping (%) 5, B.W. = 1/12 Octaves, Axis Y-base, Shaker tri-axial, ZPA = 2.2 g

ACCELEROMETER
Wilcoxon, Serial 1215, Range dB48, Location mounting plate, TT 726, Channel 2



RESPONSE SPECTRUM

FIGURE 20

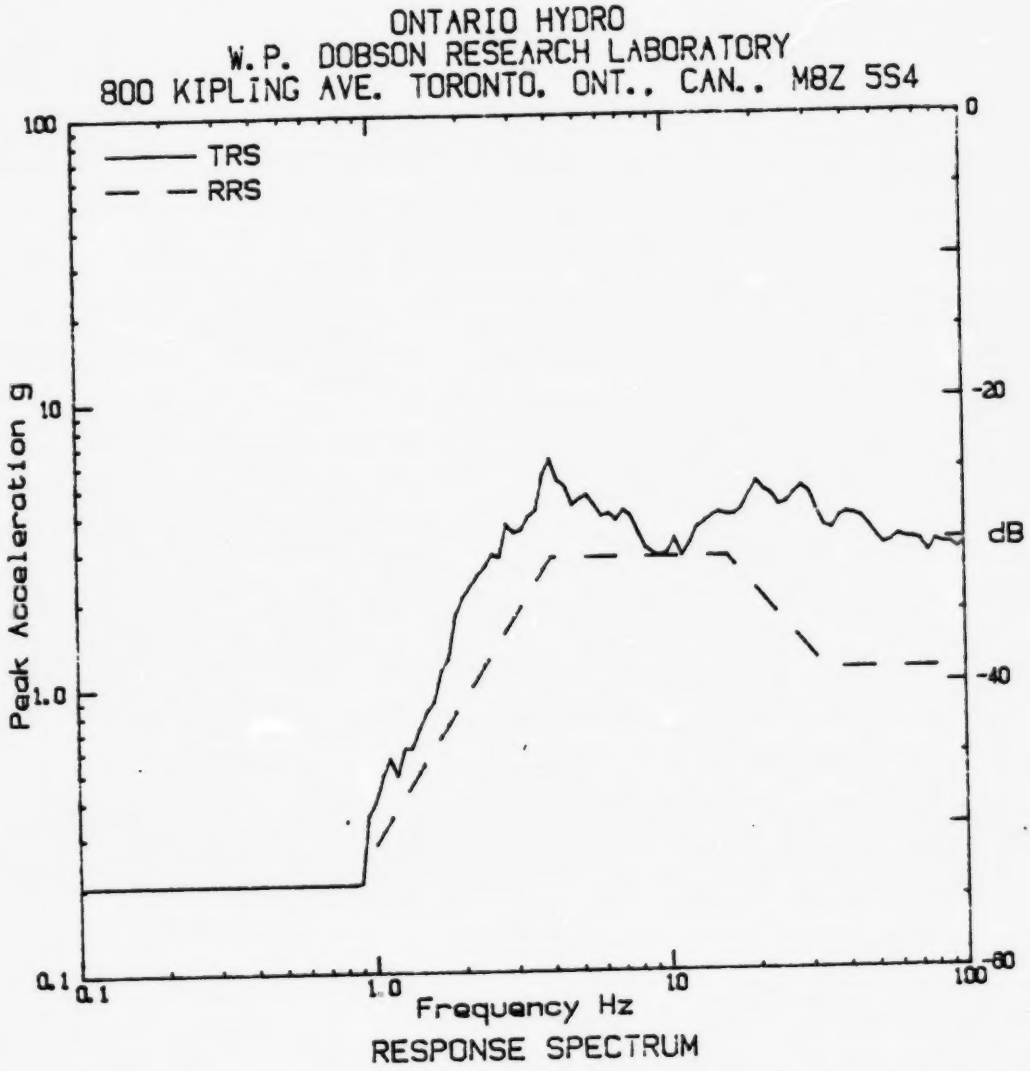
TEST ITEM
Station Cell, Exide, Model FHC 19, Cell #23

PARTICULARS
Dec. 7/84, Time 1:45, Temp('C) 24, Humidity(%) 29, Press (kPa)100.5,
Graph 5417, Record 0

SPECIFICATIONS
Spece IEEE 344, Conditions operating, table limit

ANALYSIS
Type Maximax, Damping (%)5, B.W. = 1/12 Octaves, Axis Z-base,
Shaker tri-axial, ZPA=2.5 g

ACCELEROMETER
Wilcoxon, Serial 1213, Range dB48, Location mounting plate, TT 726,
Channel 3



RESPONSE SPECTRUM

FIGURE 21

TEST ITEM
Station cells & Rack. Exide. Model FHC-19. Serial 15.23.10.
Calvert Cliffs N.P.P.

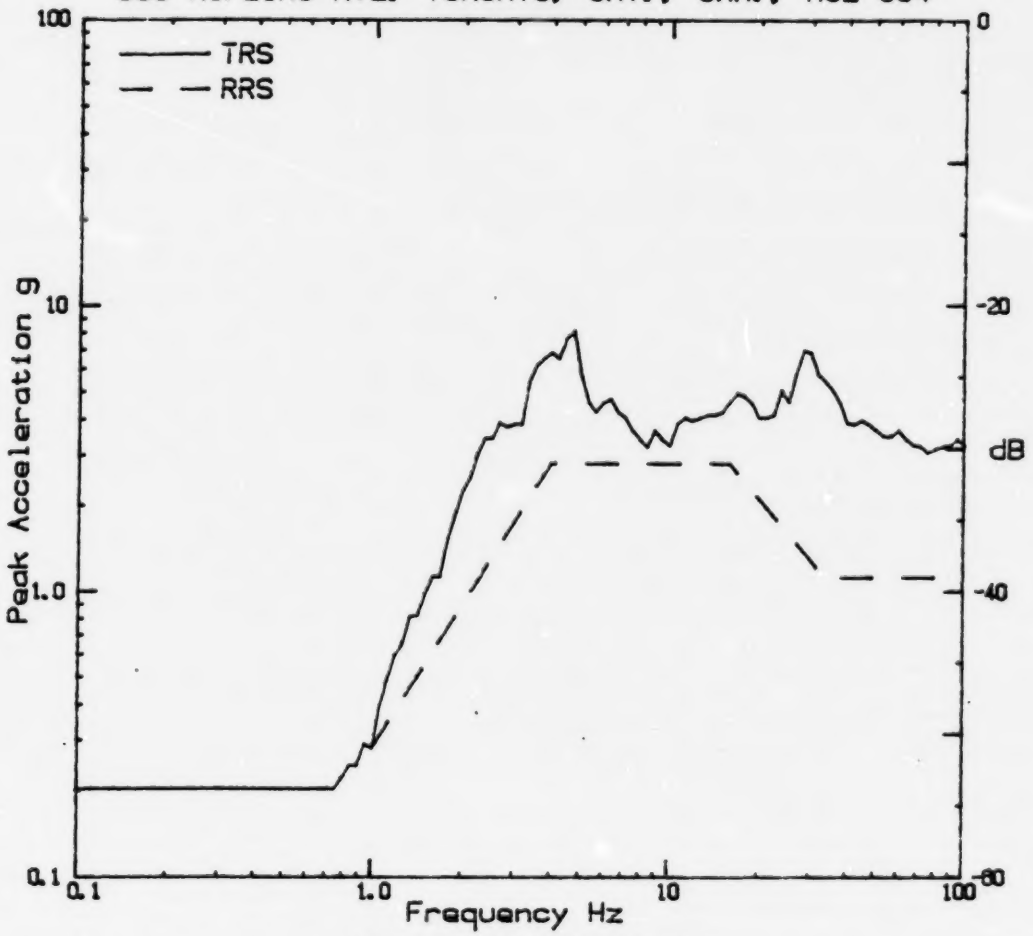
PARTICULARS
July 24/84. Time 2:44. Temp('C) 23. Humidity(%) 55. Press (kPa) 100.3.
Graph 5248

SPECIFICATIONS
Spec: IEEE 501. Conditions operating : 1 hour rate. span 7

ANALYSIS
Type Maximax. Damping (%) 5. B.W. = 1/12 Octaves. Axis X.
Shaker tri-axial. ZPA=1.13g

ACCELEROMETER
Wilcoxon. Serial S771. Range dB49. Location base-mounting plate.
Channel 1

ONTARIO HYDRO
W.P. DOBSON RESEARCH LABORATORY
800 KIPLING AVE. TORONTO, ONT., CAN., M8Z 5S4



RESPONSE SPECTRUM

FIGURE 2.2

TEST ITEM
Station cells & Rack. Exide. Model FHC-19. Serial 15.23.10.
Calvert Cliffs N.P.P.

PARTICULARS
July 24/84. Time 2:44. Temp('C) 23. Humidity(%) 55. Press (kPa) 100.3.
Graph 5250

SPECIFICATIONS
Specs IEEE 501. Conditions operating : 1 hour rate. span 7

ANALYSIS
Type Maximax. Damping (%) 5. B.W. = 1/12 Octaves. Axis Z.
Shaker tri-axial. ZPA=1.13g

ACCELEROMETER
Wilcoxon. Serial S297. Range dB49. Location base-mounting plate.
Channel 3

APPENDIX A

EARTHQUAKE MOTION AND RESPONSE SPECTRA

The way that a piece of equipment or structure responds to an earthquake will depend on the intensity of the event, and on the relationship between frequency content of the earthquake and the natural frequencies of the structure.

A convenient way of expressing the combination of intensity and frequency content of an earthquake is through the use of a graph known as a response spectrum. A response spectrum is made up by calculating the response level (acceleration, velocity or displacement) of a family of hypothetical single degree-of-freedom mechanical oscillators to the earthquake motion, and plotting these against frequency. A particular seismic "environment" is described by a set of spectra that define the response for different directions and levels of structural damping. The response of a simple structure to an earthquake can be estimated from the level of the appropriate spectra at the natural frequencies of the structure.

Response spectra deal with the response of structures to earthquake motion and contain no explicit information on the peak accelerations. However, it is known that earthquake motions is predominantly in the low frequency range (1-10 Hz) and that there will be relatively little amplification of the response of high frequency oscillators. Thus, for typical earthquake time-histories, the peak acceleration response for the oscillators at the high end of the frequency range will be quite close to the peak acceleration of the base motion from which the spectrum was generated. High frequencies correspond to short vibration periods and, in the jargon of the trade, the acceleration response t the high frequency end of the spectrum (33 Hz or above) is known as the Zero-Period Acceleration (ZPA). The ZPA is commonly taken as being equivalent to the peak acceleration of the seismic motion.

Response spectra are commonly used to define the seismic environments for structures or equipment that must survive earthquakes. Unless there is a large amount of site-specific data available, the spectra specified for a particular project are normally based on standard curves that have been developed to represent a broad range of possible conditions. The spectral curve defined in IEEE 501 /11/ is typical. This standard specifies the relative intensity of the spectrum over the frequency range. The absolute intensity will depend on site conditions. For convenience, the absolute intensity is expressed as the ZPA.

When a particular piece of equipment is seismically qualified to IEEE 501, the test response spectra (ie. the response spectra calculated from the test motions) will be compared to the standard shape. The qualified level is the ZPA of the normalized curve that lies just below the test spectrum over the seismic frequency range (1-33 Hz).

For an efficient test, the test spectrum should closely match the standard spectral shape. However, in practical testing, the experimental curve will often "overshoot" the desired curve over certain frequency ranges. This may be because of mechanical limitations in the test rig. For example, the shaker table used in this series of tests has a limited stroke (displacement) so that it s difficult to generate very high response levels at low frequencies. Thus, when the rig is run at high power levels, the test motions often produce response spectra which are high in the high frequency range (above 5 Hz) and low at low frequencies, relative to the standard IEEE 501 shape. When these test spectra are fitted to the standard shape by strict rule, the result is a considerable overshoot for much of the high frequency range. This means that the ZPA taken from the standard curve is far below the peak accelerations that were actually encountered.

As mentioned above, the standard shape was developed to represent a broad range of seismic conditions, structural supports and low frequencies so that equipment with low natural frequencies will be adequately tested. However, in the case of the battery cells and racks, all of the structural modes of vibration have been found to have relatively high natural frequencies. This means that these devices will not be significantly effected by the low frequency component of the input motion. We believe that it is reasonable in this case to ignore the low frequency end of the experimental spectra and to fit the standard shape over a frequency range of 4-33 Hz. This has the effect of increasing the ZPA of the standard curve to a value that more accurately reflects the maximum accelerations encountered in each test.